

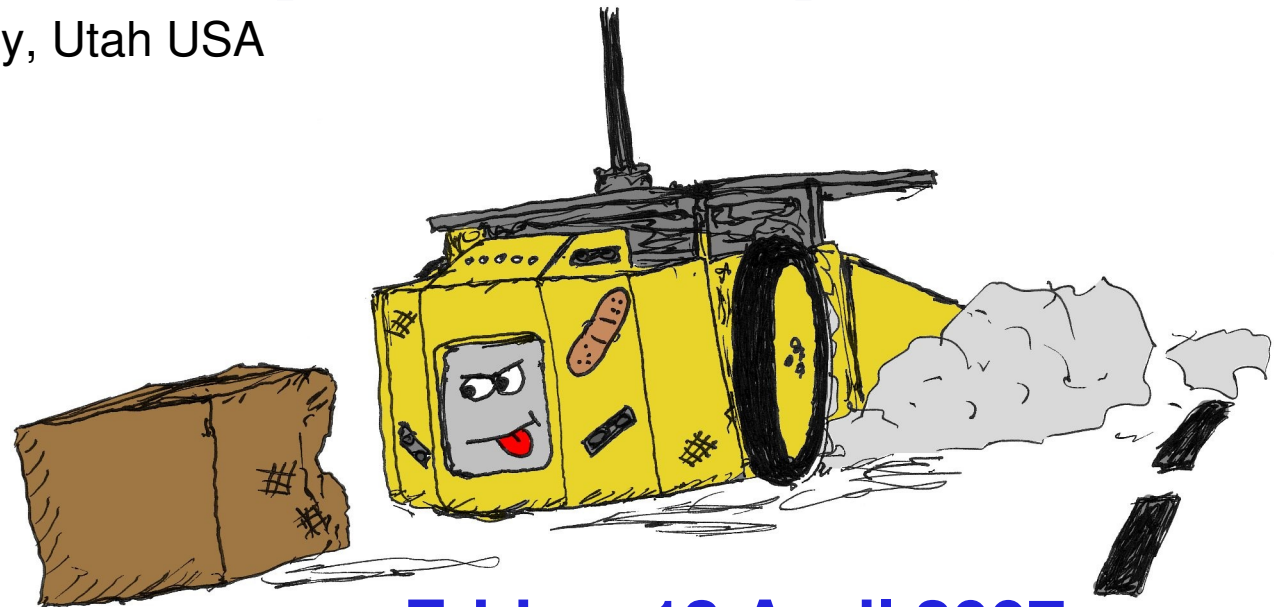
Remote Low Frequency State Feedback Kinematic Motion Control for Mobile Robot Trajectory Tracking



Daniel Montrallo Flickinger

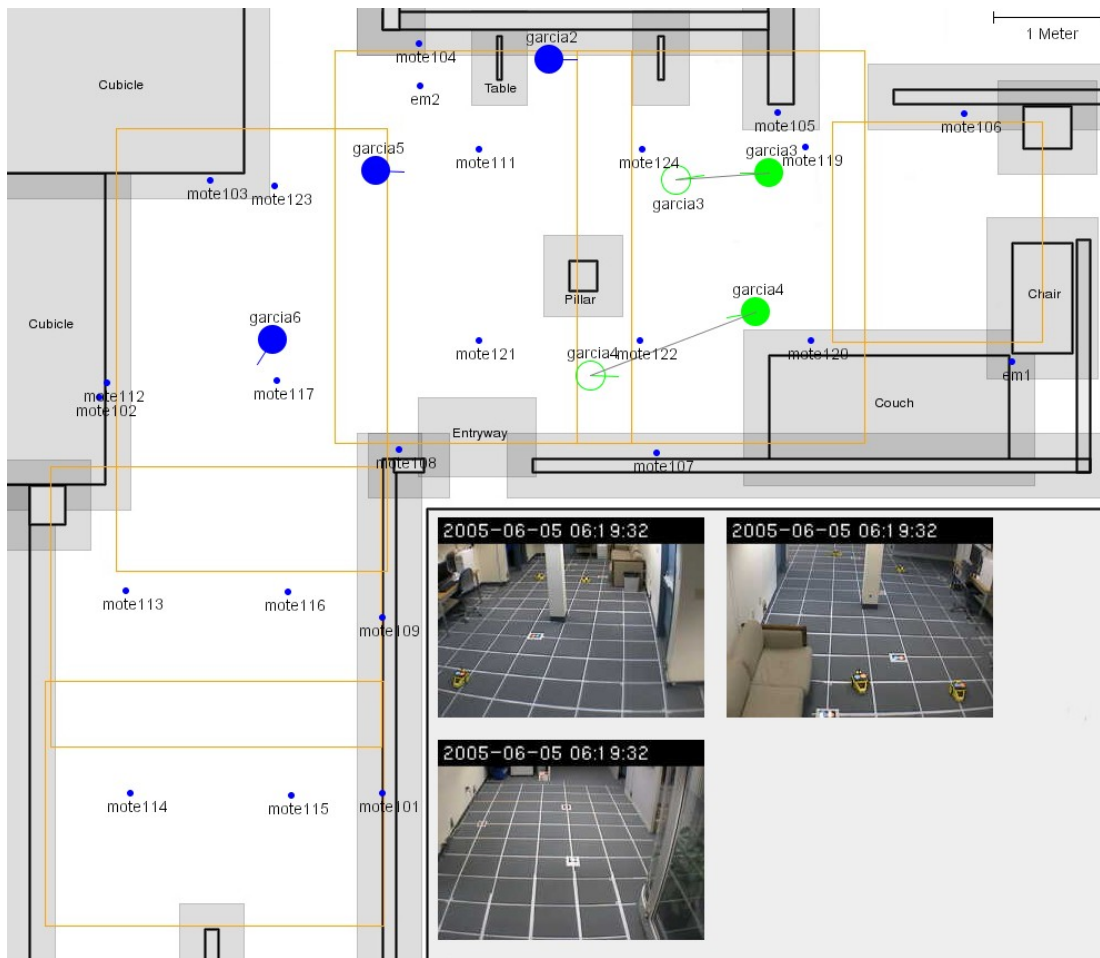
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Mobile Emulab



Example of the user control interface

- Mobility is added to Emulab, a wireless research testbed.
- Uses robots to position antennas within a semi-controlled environment
- Publicly available to remote users via the Internet
- Used for wireless network experiments

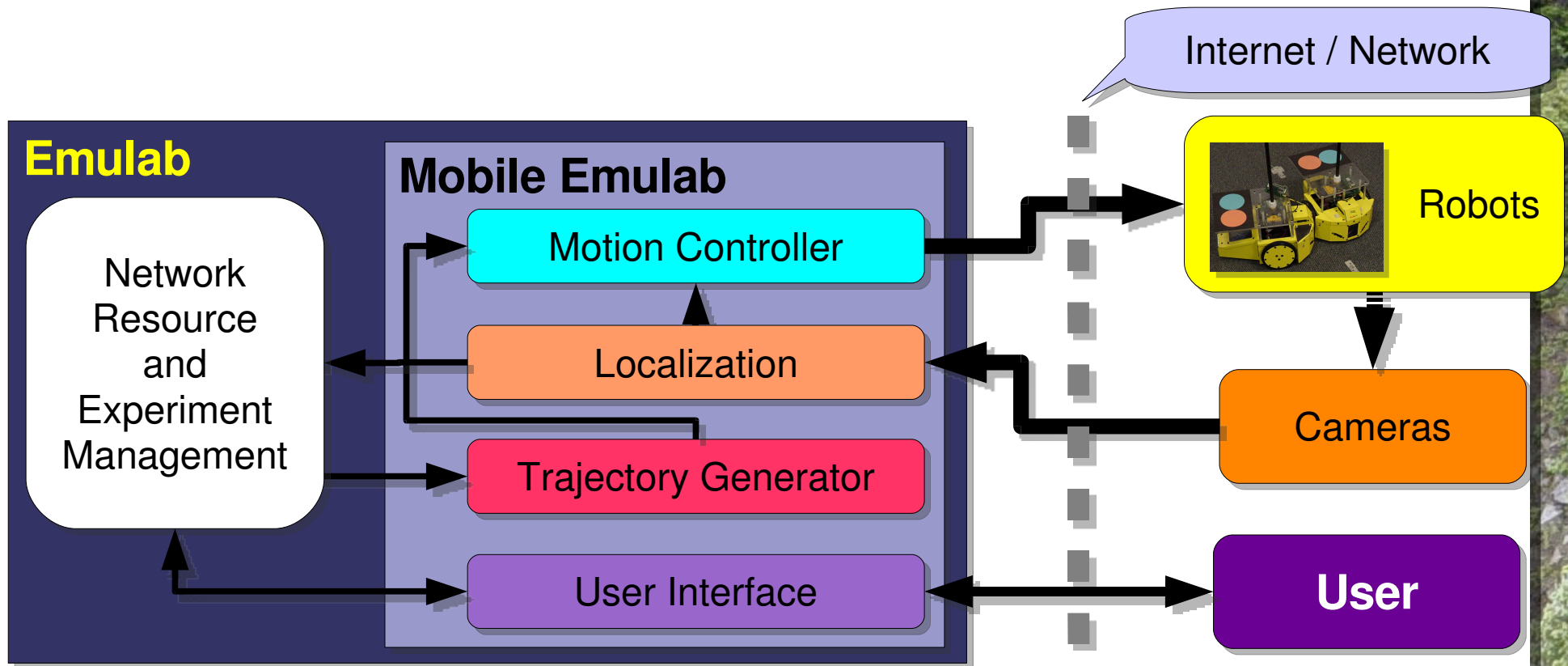
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System Architecture



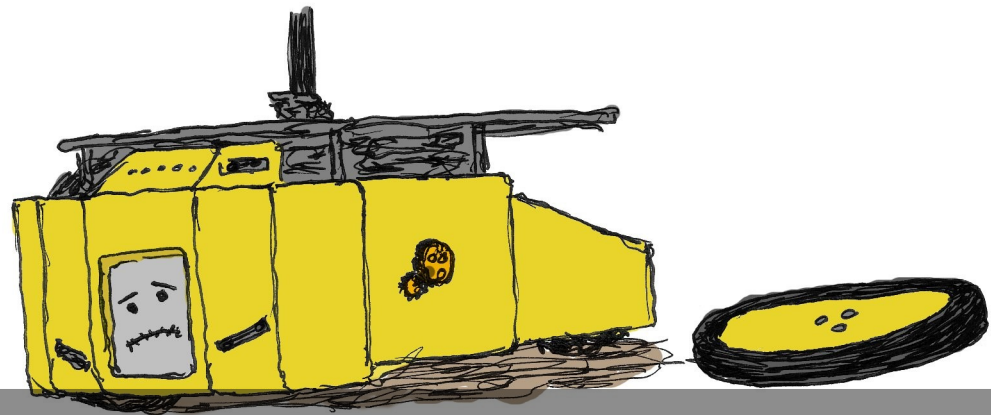
Goals

- Teleoperated system that removes the entire motion control structure from the robot, in order to preserve the availability of crucial onboard resources
- Centrally controlled, medium scale mobile robots for wireless networking experiments
- Kinematic motion control at low frequency

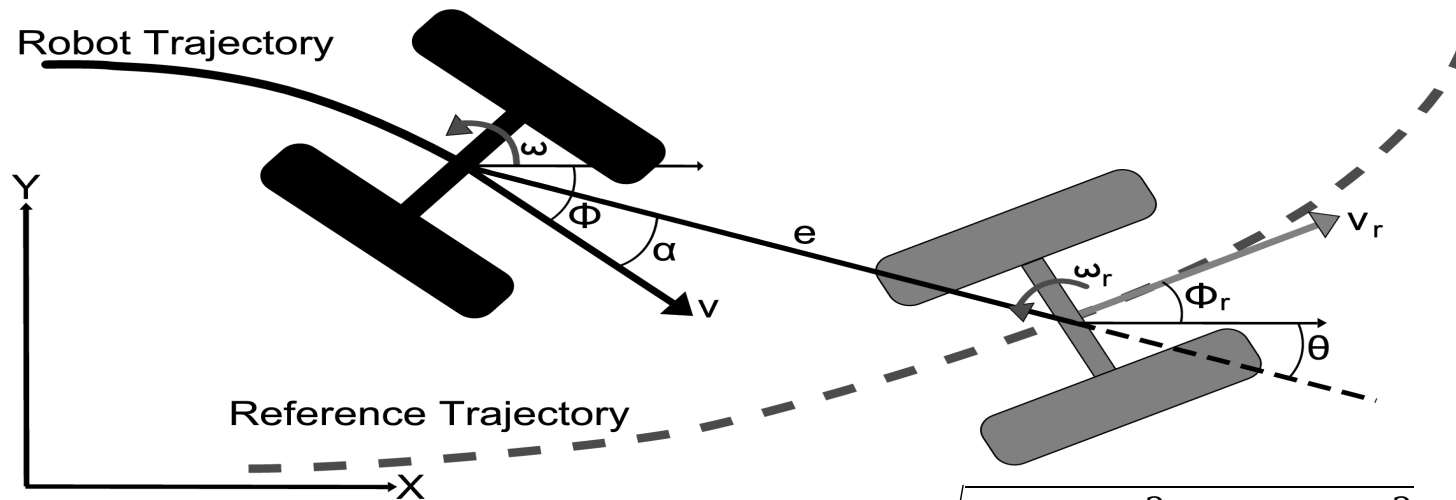


Challenges

- The majority of on board computer resources must be kept available for experimenters
- Kinematic control (Built in API to send wheel velocity commands)
- Robots can receive velocity commands at 50 Hz maximum
- Centralized localization system (Odometer drift is significant)
- Localization data limited to 30 Hz, not periodic (Camera hardware cost)



Kinematics



$$e = \sqrt{(x - x_r)^2 + (y - y_r)^2}$$
$$\theta = \text{Atan}(-y - y_r, -x - x_r)$$
$$\alpha = \theta - \phi + \phi_r$$

- Polar form, which satisfies Brockett's Theorem
- Cartesian to Polar conversion required to obtain polar states

Trajectory Tracking Controller

Controller: (Bounded velocity, curvature.)

$$v_d = \frac{k_1 \cdot e \cdot k_e \cdot \tanh(e - r\sqrt{2} \cdot k_e) + v_r \cdot e \cdot \cos(\theta) \cdot k_e + v_r \cdot r\sqrt{2} \cdot \sin(2\theta) \cdot (\sin(\theta) + \frac{\omega_r}{v_r} \cdot e)}{e \cdot k_e + r\sqrt{2} \cdot \sin(2\theta) \cdot \sin(\alpha)}$$

$$\omega_d = k_2 \cdot \tanh(\theta + \alpha) + 2\dot{\theta} + \dot{\phi}_r$$

$$k_e = \sqrt{(\zeta - \cos 2\theta)}$$

Dynamic Extension: (Controller outputs become new states.)

$$\dot{v} = -k_v(v - v_d) + \dot{v}_d \quad \dot{\omega} = -k_\omega(\omega - \omega_d) + \dot{\omega}_d$$

X. Zhu, Y. Kim, and M. A. Minor, "Cooperative distributed robust control of modular mobile robots with bounded curvature and velocity," in 2005 IEEE/ASME International Conference on Advanced Intelligent Mechatronics, Monterey, California, 2005.

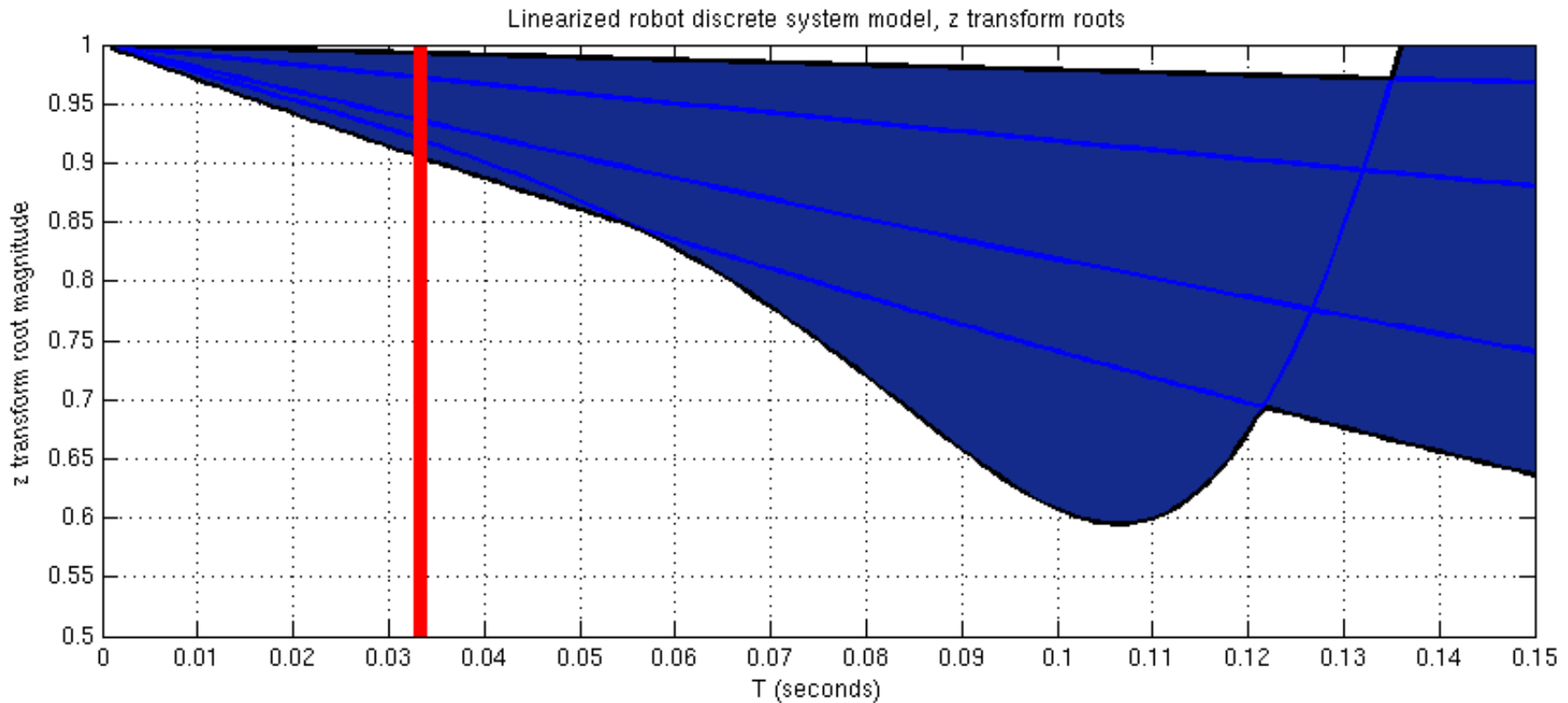
Stability Analysis

- Define new error states: $e_v = v_r - v_a$ $e_\omega = \omega_r - \omega_a$
- Substitute new states into control laws
- Substitute control laws into kinematic system equations
- Linearize about an equilibrium point (Polar states @ 0, with desired velocity)
- Make the linear system discrete
- Approximate the state transition matrix with a 4th order Taylor series
- Solve for roots, and tune control gains for specified root and damping values

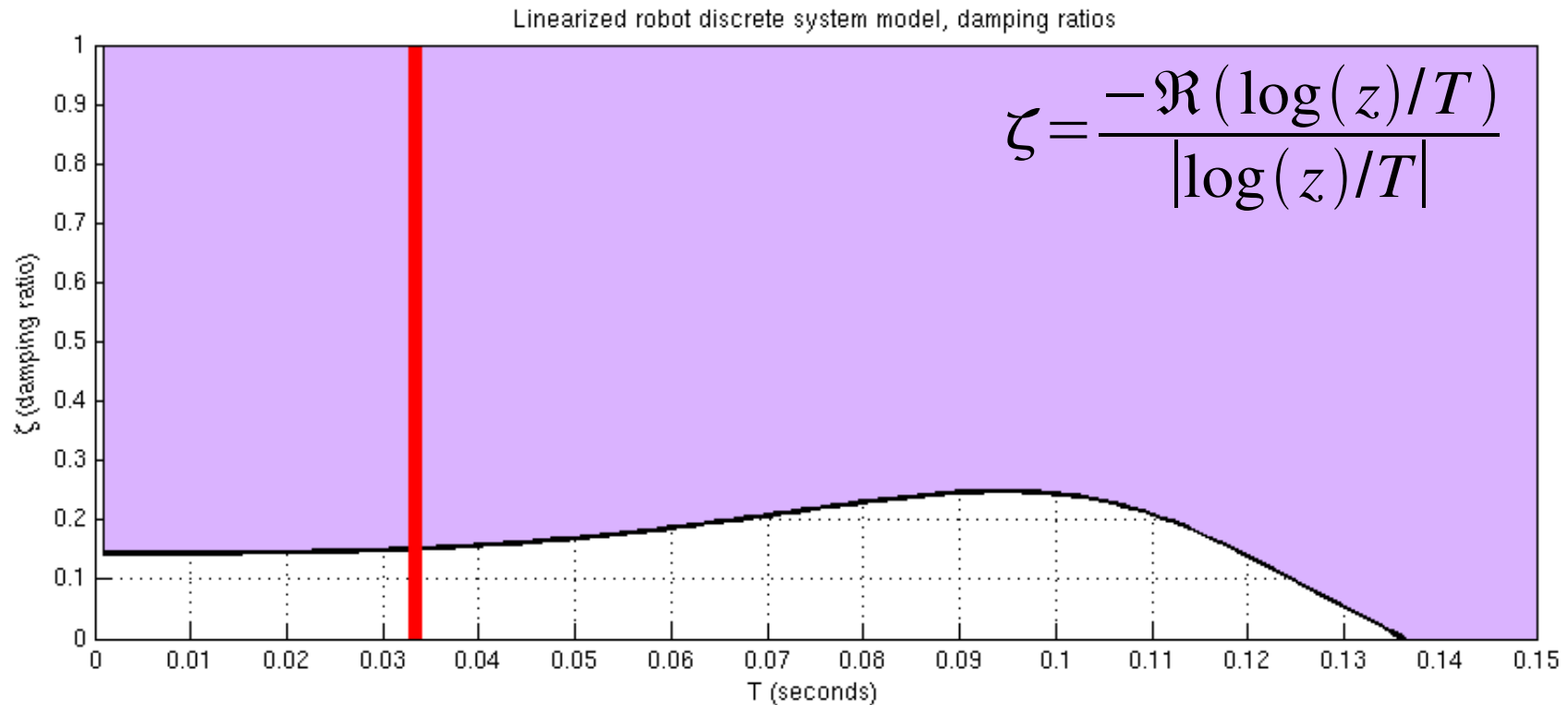
$$r = 0.02 \text{ m}, \varepsilon = 0.003 \text{ m}, k_1 = 0.85, \\ k_2 = 0.3, \text{ and } k_v = k_\omega = 3.0.8$$



Stability Analysis: Roots

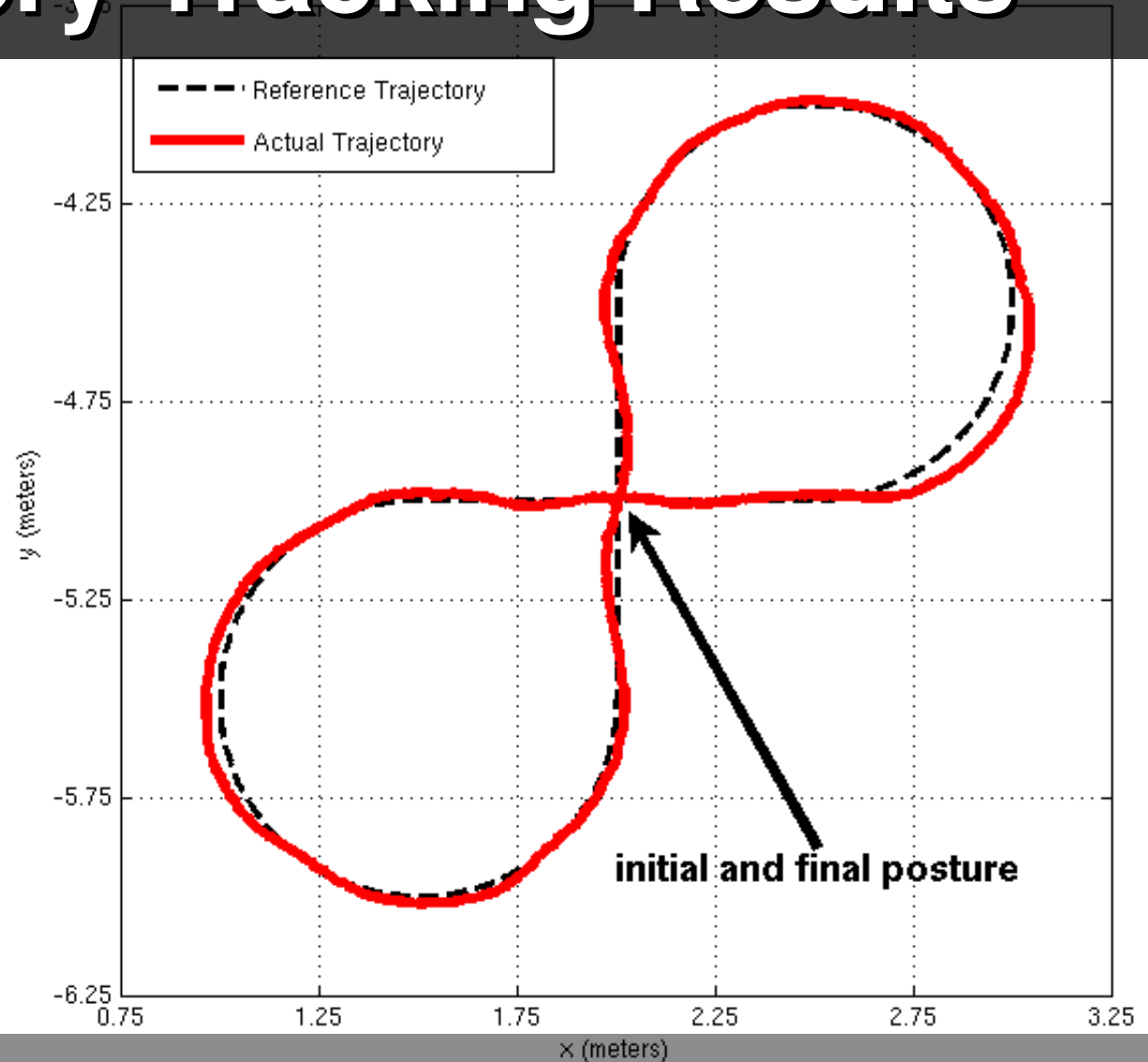


Stability Analysis: Damping Ratio



Trajectory Tracking Results

- Tracking error less than 100 mm
- Reference velocity of 0.1 meters per second
- Experiment featured in the video attachment



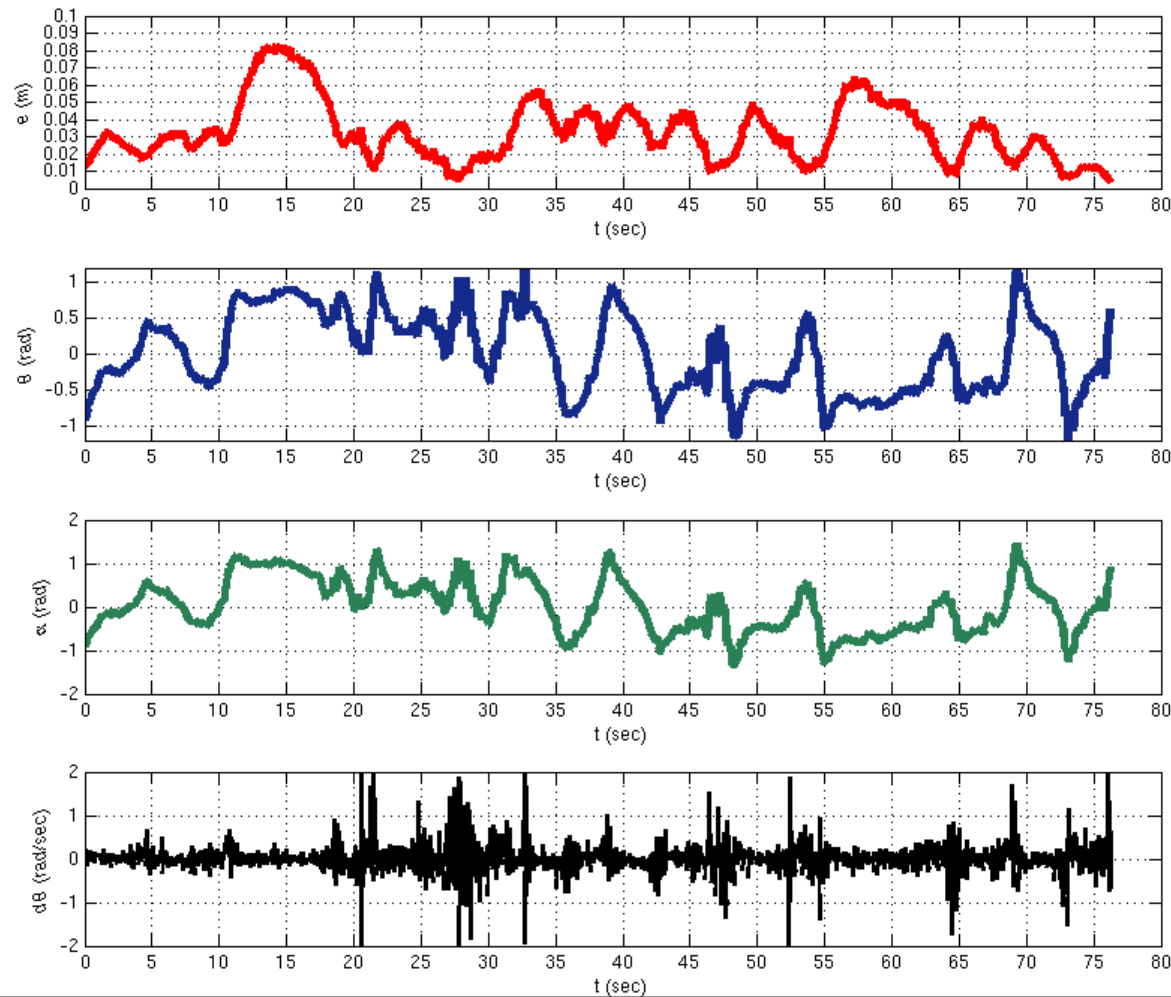
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System Response



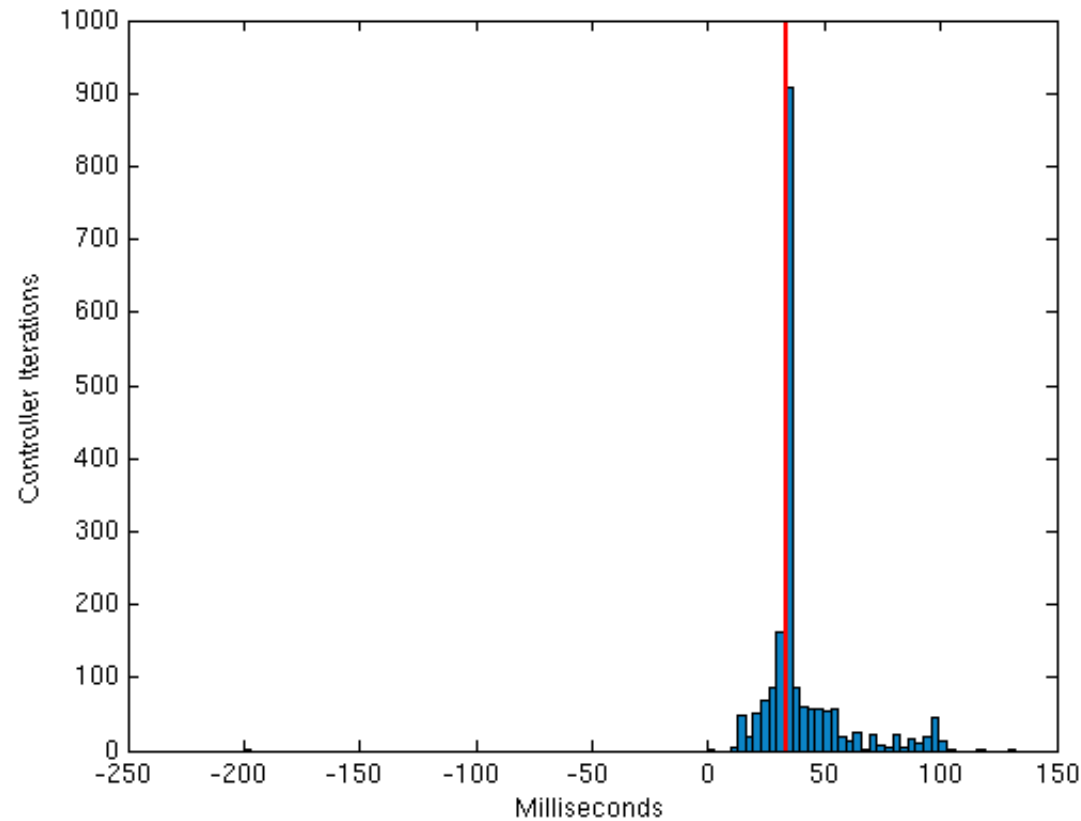
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Localization Data Frequency



Conclusion

- Kinematic control for wheeled mobile robot trajectory tracking achieved at low sampling frequency
- Stability analysis on discrete linear system for gain tuning
- Motion control over a noncontrolled network

Future Work

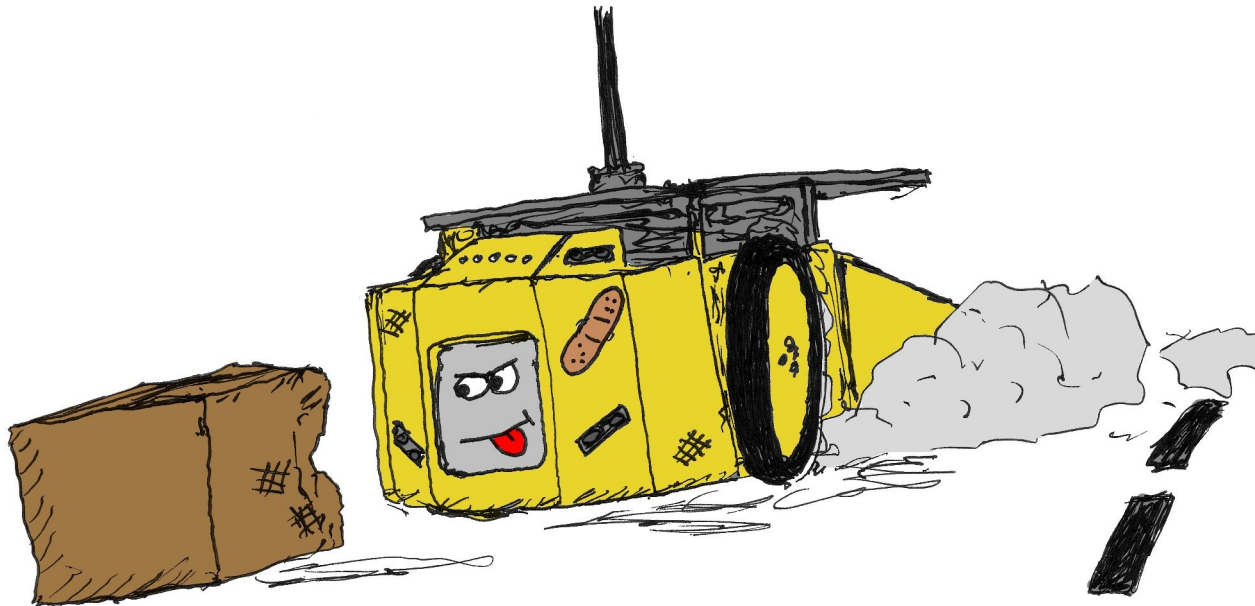
- Design a discrete nonlinear controller instead of adapting a continuous controller
- Implement C^2 continuous trajectories to minimize effects of curvature discontinuities

Acknowledgments

- Thanks to:
 - Mark Minor and Youngshik Kim for help on the discrete system stability analysis
 - Youngshik Kim for the design of the state feedback controller used in this work for trajectory tracking
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Thank you.



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